BEFORE THE ILLINOIS POLLUTION CONTROL BOARD

IN THE MATTER OF:)	
)	
PROPOSED AMENDMENTS TO)	
EXEMPTIONS FROM STATE)	
PERMITTING REQUIREMENTS)	
FOR PLASTIC INJECTION MOLDING)	R 05 -20
OPERATIONS)	
(35 Ill. Admin. Code 201.146))	

PRE-FILED TESTIMONY ON BEHALF OF THE CHEMICAL INDUSTRY COUNCIL OF ILLINOIS

In response to questions posed at the first hearing in this matter on July 1, 2005, CICI is herewith providing certain requested information. CICI witnesses, Lynne Harris, Lisa Frede, and Patricia Sharkey, will be present to answer questions regarding these responses at the July 15, 2005 hearing in Springfield.

1. Size of Facilities Exempted Under This Proposal

At the July 1, 2005 hearing, the Board asked how many PIM machines may be located at a given PIM facility. CICI has not found any studies or data directly addressing this question. However, CICI can state that its member facilities have between 4 and 70 machines.

Because the size of PIM machines varies, resin throughput is a better indicator of the volume of emissions associated with a given facility. CICI member facilities have annual PIM resin throughput ranging from 100 tons/yr to 3,250 tons/yr. Average facility annual PIM resin throughput is approximately 500 tons/yr.

2. Estimated Volume of PIM Emissions Statewide in Illinois.

The Board asked what volume of emissions would be exempt from permitting under this exemption. A broad estimate of the total volume of emissions generated by PIM processes statewide can be derived by first multiplying the number of facilities in Illinois by the average volume of resin processed per facility, and then multiplying that number by an appropriate emission factor. As indicated in Mr. Harris' testimony, a worst case VOM emission factor is 0.4 lb/ton of resin processed. If we add to that a worst case emission factor of 0.4 lb/ton of resin processed for the use of release or cleaning agent, as discussed in Section 5 below, we arrive at a conservative overall VOM emission factor of 0.8 lb/ton of resin used.

Using the above information and the previous testimony that approximately 500 PIM facilities are located in Illinois, the formula for calculating statewide VOM emissions associated with PIM is as follows:

500 facilities X	500 tons resin /yr $=$	250,000 tons resin /yr
250,000 tons/yr X	0.8 lb VOM /ton resin =	100 tons VOM /yr

CICI believes *100 tons per year* is a reasonable worst case estimate of the total volume of VOM emissions generated statewide by PIM facilities in Illinois. We note that this equates to *0.2 tons of VOM emissions per facility per year*. We further note that not all of the approximately 500 PIM facilities in Illinois will be exempted from state permitting under the proposal in this rulemaking. In response to the Board's question regarding the number of PIM facilities that have no other processes, such as coating, SPI did a rough survey of its members and determined that approximately 80% of its members in the PIM industry do not perform other processes at the their facilities. This

indicates that around 20% of the approximately 500 Illinois PIM facilities will not be covered by this exemption. Thus total statewide emissions of VOM covered by this exemption are actually likely to be on the order of 80 tons per year.

To answer any concern the Board may have that there may be larger volumes of emissions involved, CICI has proposed in its Second Errata Sheet to limit the proposed exemption to PIM facilities with no more than 5,000 tons/yr of resin processed. If every facility in Illinois processed 5,000 tons of resin per year (an extraordinary assumption), the total VOM emissions subject to this exemption would be 1,000 tons/yr. That equates to approximately 2 tons of VOM per year per facility.

3. Location of PIM facilities in Illinois (Attainment Areas/ Non-Attainment Areas)

The Board asked about the location of PIM facilities in the State and whether they were primarily located in Attainment or Non-Attainment Areas. To answer this question, CICI reviewed the locations of the Illinois facilities listed in the Plastic News "2005 Survey of North American Injection Molders" and the locations of CICI member facilities, and determined that 14% of those PIM facilities are located in Attainment Areas and the remaining 86 % are located in Non-Attainment Areas. Of those located in Non-Attainment Areas, all are located in areas which have been designated as Moderate NAA under the new 8-hour ozone standard.

4. Estimated Emission from Resin Handling Operations: Loading, Unloading, Conveying, Storage, Mixing, Grinding, Drying

As indicated at the July 1st hearing, CICI has attempted to find studies and other sources of information on the volume and type of emissions generated by the various activities associated with resin handling operations. We have found no studies directly

addressing or quantifying emissions from these activities. This is actually not surprising. As indicated in Mr. Harris' June 16, 2005 Pre-Filed Testimony, emissions from the injection molding process as a whole had not been quantified prior to 1996. This lack of quantitative information on emissions may also be explained by the nature of the materials involved and the process. The resin and scrap are hardened plastic material at ambient and low temperatures. Furthermore, these ancillary activities operate under negative pressure, thus emissions from the movement of resin, the drying of the resin and the grinding of scrap plastic are largely, if not entirely, drawn back into the process.

The following information on how and where emissions are formed in this process may assist the Board in understanding that emissions from these ancillary activities are minimal.

a. VOM and HAP Emissions

VOM and HAP emissions from plastic resin are directly related to temperature. As found in the SPI studies accompanying Mr. Harris' Pre-Filed Testimony (Group Exhibit 3), "emission rates are directly correlatable with the melt temperature of the resin involved." (Group Exhibit 3, Harris Exhibit 3, p. 56.) Thermoplastic resins have melt temperatures in the range of 300 F – 600 F. (Group Exhibit 3, Harris Exhibits 3 – 6.) The SPI studies demonstrate that even at the melt temperatures reached in the extruder screw VOM and HAP emissions are low. Thus, the brief drying of the resin at far lower temperatures to remove moisture from the pellets can be presumed to generate only a fraction of those emissions. The ancillary resin loading, conveyance and mixing at ambient temperatures can be presumed to be even lower.

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To a varying degree, all plastic resins take on moisture when exposed to relative humidity. Even a minimal amount of moisture in many plastics can negatively affect molding characteristics. Dryers operated at low temperatures are often utilized to remove such moisture from plastic resin prior to the plastic injection molding process. The dryers blow heated ambient air over the plastic resins. The temperatures used for drying plastic resins are generally less than one half of the melting temperature of the plastic resin involved. (See attached Table 5.1 from the *Modern Plastics Handbook*.) Although CICI has not been able to find any data on emissions from dryers, emissions of VOM from plastic resin at the relatively low temperatures used in the drying process can be presumed to result in a small percentage of VOM or particulate emissions generated by the overall process.

The conclusion that VOM emissions from resin pellets handled at ambient temperatures are minimal is confirmed by the polyethylene study (Group Exhibit 3, Harris Exhibit 5) which measured emissions of VOC from the hopper area and found that emissions from this area accounted for less than 2% of the total VOCs measured. (<u>Id.</u>, p. 577.)

b. Particulate Matter Emissions

There is an assumption that the movement of resin, even at ambient temperatures, generates some level of particulate matter ("PM"). However, CICI has been unable to find any EPA or industry studies of this subject.

To provide the Board with some perspective on the level of PM present at a PIM facility, CICI Regulatory Affairs Director Lisa Frede visited one of its member facilities on July 7, 2005. Ms. Frede will provide testimony at the July 15, 2005 hearing that she

found it to be exceedingly clean, with no dust or film on the floor or the equipment, including the grinder or granulator, which is presumed to be the piece of equipment most likely to produce PM. She will also testify that none of the employees in this workplace wear respiratory protection, indicating the indoor particle levels meet OSHA standards without such protection. One of the primary reasons that PM is so low in these facilities is that product specifications require that foreign material not enter the process. Another reason is that injection molding and the associated resin and scrap handling are almost entirely enclosed operations which take place under negative pressure.

Ms. Frede will provide photographs and her observations on the injection molding process. (See attached Photos Nos. 1 - 9.) As can be seen from the attached photographs, the resin is brought to the machine in a cardboard "gaylord" box and fed via vacuum hose into the dryer and the hopper. The screw extruder and the mold are entirely enclosed processes. When the mold opens, the product drops on to an open conveyor belt, which can be seen to have little or no dust on it. Ms. Frede will testify that the plastic product and plastic scrap leaving the mold are extremely clean. The scrap plastic "runners" and "sprus" are removed from the mold by way of a robotic arm which drops the scrap into the grinder or granulator. As can be seen from the attached photos, the grinder area has little or no dust. Again, this is because the grinder operates under negative pressure and both the scrap plastic and any associated dust are drawn into the grinder. Closing the loop, the granulated plastic, while somewhat dusty, is fed directly from the grinder back to the hopper to be reused in the process. This takes place by way of a vacuum hose.

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Given the fact that these processes are so clean, there is little likelihood that PIM machines would be vented outside the workplace. CICI's survey of its member facilities indicates that none of those facilities vent PIM machines outside the workplace. Thus there is little likelihood of PIM emissions entering the outside environment. To the extent that a PIM facility has emissions of concern within the workplace, they are subject to OSHA standards and are not regulated under the Environmental Protection Act or air pollution control permits issued under the Board's rules.

At the July 15, 2005 hearing, Ms. Frede will be happy to answer any questions regarding her observations at this facility. CICI will also provide samples of a typical resin, typical "runner" and granulated scrap, and a typical PIM plastic product which Ms. Frede observed being handled and processed at this facility.

5. Mold Release Agents and Cleaning Agents

Mold release agent and/or mold cleaner are sometimes used in the plastic injection molding (PIM) process. Mold release agent leaves a very thin layer of a "nonstick" substance on the surface of the mold to help parts fall from the mold as it opens at the end of the cycle. Mold cleaner is used to remove built-up residue from the mold surface. Some CICI member facilities have designed their molds to avoid use of mold release altogether, but still use mold cleaner.

Historically, the volatile organic matter content of aerosol mold release agents and mold cleaning products was in excess of 90%. However, mold release agents and mold cleaning products are now available in water-based formulations and in formulations that utilize non-photochemically reactive chemicals as carrier solvents.

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Both mold release agent and mold cleaner are generally used in 12- 16 ounce aerosol cans. Based on data collected from CICI member facilities, VOM emissions from mold release agent and/or mold cleaner range from less than 0.1 lbs/ton of resin processed up to 0.4 lb/ton of resin processed. The combined usage of mold release agents and mold cleaner at a PIM facility can be conservatively estimated to generate 0.4 lbs of VOM per ton of resin processed.

In general, facilities try to design molds to minimize the use of mold release agents and mold cleaner because it is very inefficient to stop the PIM machine periodically to apply either release agent or cleaner to the mold. Well-designed molds require only a minimal amount of either substance. When possible, facilities try to apply mold release agent or mold cleaner only at the beginning of a production shift.

6. Definitions of "Compression Molding" and "Transfer Molding"

In response to a question from the Board, CICI is providing the following

definitions which appear on The Society of the Plastics Industry, Inc. ("SPI") website at

http://www.plasticsindustry.org.:

"Compression molding is the most common method of forming thermosetting materials. It is not generally used for thermoplastics.

"Compression molding is simply the squeezing of a material into a desired shape by application of heat and pressure to the material in a mold.

"Plastic molding powder, mixed with such materials or fillers as woodflour and cellulose to strengthen or give other added qualities to the finished product, is put directly into the open mold cavity. The mold is then closed, pressing down on the plastic and causing it to flow throughout the mold. It is while the heated mold is closed that the thermosetting material undergoes a chemical change which permanently hardens it into the shape of the mold. The three compression molding factors -- pressure, temperature and time the

mold is closed -- vary with the design of the finished article and the material being molded."

"Transfer molding is most generally used for thermosetting plastics. This method is like compression molding in that the plastic is cured into an infusible state in a mold under heat and pressure. It differs from compression molding in that the plastic is heated to a point of plasticity before it reaches the mold and is forced into a closed mold by means of a hydraulically operated plunger.

"Transfer molding was developed to facilitate the molding of intricate products with small deep holes or numerous metal inserts. The dry mold compound used in compression molding sometimes disturbs the position of the metal inserts and the pins which form the holes. The liquefied plastic material in transfer molding flows around these metal parts without causing them to shift position."

As stated in the first hearing, CICI is no longer proposing that these processes be

included in the proposed exemption and does not plan to provide additional testimony

regarding these processes.

Dated: July 11, 2005

Respectfully submitted,

CHEMICAL INDUSTRY COUNCIL OF ILLINOIS

By: <u>/s/ Patricia F. Sharkey</u> One of its Attorneys

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NOTICE OF FILING

TO: Ms. Dorothy M. Gunn Clerk of the Board Illinois Pollution Control Board 100 West Randolph Street Suite 11-500 Chicago, Illinois 60601 (VIA ELECTRONIC FILING)

(PERSONS ON ATTACHED SERVICE LIST)

PLEASE TAKE NOTICE that on July 11, 2005, I filed with the Office of the Clerk of the Illinois Pollution Control Board by electronic filing the SECOND ERRATA SHEET and PRE-FILED TESTIMONY ON BEHALF OF THE CHEMICAL INDUSTRY COUNCIL OF ILLINOIS, a copy of which is hereby served upon you.

Dated: July 11, 2005

Respectfully submitted,

CHEMICAL INDUSTRY COUNCIL OF ILLINOIS

By: <u>/s/ Patricia F. Sharkey</u> One of its Attorneys

Patricia F. Sharkey Mayer, Brown, Rowe & Maw LLP 71 South Wacker Drive Chicago, Illinois 60606-4637 (312) 782-0600

CERTIFICATE OF SERVICE

I, Patricia F. Sharkey, an attorney, hereby certify that I have served the Second Errata Sheet and Pre-Filed Testimony on Behalf of the Chemical Industry Council of Illinois upon:

Ms. Dorothy M. Gunn Clerk of the Board Illinois Pollution Control Board 100 West Randolph Street Suite 11-500 Chicago, Illinois 60601 (Electronic Mail)

Matthew Dunn, Chief Division of Environmental Enforcement Office of the Attorney General 188 West Randolph Street, 20th Floor Chicago, Illinois 60601 (U.S. Mail)

Donald Sutton Manager, Permit Section Division of Air Pollution Bureau of Air Illinois Environmental Protection Agency 1021 North Grand Avenue East Post Office Box 19276 Springfield, Illinois 62794-9276 (U.S. Mail) Charles E. Matoesian Division of Legal Counsel Illinois Environmental Protection Agency 1021 North Grand Avenue East Post Office Box 19276 Springfield, Illinois 62794-9276 (U.S. Mail and E-Mail)

Office of Legal Services Illinois Department of Natural Resources One Natural Resources Way Springfield, Illinois 62702-1271 (U.S. Mail)

as indicated above, by e-mail and/or by depositing said document in the United States Mail, postage prepaid, in Chicago, Illinois on July 11, 2005.

<u>/s/ Patricia F. Sharkey</u> Patricia F. Sharkey

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<u>CHEMICAL INDUSTRY COUNCIL OF ILLINOIS'</u> <u>SECOND ERRATA SHEET</u>

The Chemical Industry Council of Illinois ("CICI"), by its attorneys Mayer,

Brown, Rowe & Maw LLP, hereby submits the following corrections and amendments to

documents previously filed in this proceeding:

AMENDMENT TO PROPOSED REGULATORY LANGUAGE

CICI proposes to amend the text of its regulatory language, as proposed in its

original filing on April 19, 2005, as follows:

TITLE 35: ENVIRONMENTAL PROTECTION SUBTITLE B: AIR POLLUTION CHAPTER I: POLLUTION CONTROL BOARD PART 201 PERMITS AND GENERAL PROVISIONS

Section

201.146 Exemptions from State Permit Requirements

Construction or operating permits, pursuant to Sections 201.142, 201.143, and 201.144 of this Part, are not required for the classes of equipment and activities listed below in this Section. The permitting exemptions in this Section do not relieve the owner or operator of any source from any obligation to comply with any other applicable requirements, including the obligation to obtain a permit pursuant to Sections 9.1(d) and 39.5 of the Act, Sections 165, 173, and 502 of the Clean Air Act or any other applicable permit or registration requirements.

* * *

hhh)Plastic injection, compression, and transfer molding equipment with an annual
through-put not exceeding 5,000 tons of plastic resin and associated plastic
resin handling, loading, unloading, conveying, mixing, storage, grinding,
granulating, and drying equipment and associated mold release and mold
cleaning agents.

Respectfully submitted,

CHEMICAL INDUSTRY COUNCIL OF ILLINOIS

By: /s/ Patricia F. Sharkey One of Its Attorneys

Dated: July 11, 2005

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Charles A. Harper Editor in Chief

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5.6 Chapter Five

TABLE 5.1	Suggested Drvi	na Conditions for	Generic Resins ^{3,4}
TADLE J. I	Suggested Dry	ng conditions io	Generic nesilis

Material	Water absorption, %	Maximum water, %	$T_{ m extrusion}, ^{\circ}{ m C}$	$T_{\text{inj. molding,}}$ °C	T_{drying}	t _{drying} , h
Acrylonitrile						
butadiene						
styrene						
(ABS)	0.25 - 0.40	0.20	225	260	88	3-4
Acetal	0.25	_	_	200	93	1 - 2
Acrylic	0.20-0.30	0.08	190	235	82	1-2
Polyamide-6						
(nylon)						
(PA-6)	1.60	0.15	270	290	82	4-5
Polyamide-6, 6 (nylon)	1.00	0.10	210	200	01	
(PA-6,6)	1.50	0.15	265	265	82	4-5
Polycarbonate	1.00	0120	200	200	02	
(PC)	0.20	0.02	290	300	120	3-4
Polybutylene	0.20	0.02	200	000	120	0-1
terephthalate (PBT)	0.08	0.04		240	125	2-3
Polyethylene	0.00	0.01		210	140	20
terephthalate (PET)	0.10	0.005	250	255	160	4–5
Polyetherimide (PEI)	0.25	0.000	200	370	155	4-5 4-5
High-density	0.20			510	100	4-0
polyethylene (HDPE)	< 0.01		210	250		
Low-density	<0.01	—	210	200		—
polyethylene (LDPE)	< 0.01		180	205		
Linear low-density	<0.01	_	100	200	_	_
polyethylene						
(LLDPE)	< 0.01		260	220		
Polyphenylene	<0.01		200	220	_	_
oxide (PPO)	0.07		250	275	100	2–3
Polypropylene (PP)	< 0.01		235	255	100	2-3
Polystyrene (PS)	0.03	_	233	220	_	
High-impact	0.05		210	220		
polystyrene (HIPS)	0.10		235	230		
	0.10	_	230	230	-	
Polyphenylene				330	140	
sulfide (PPS)	0.30	0.05	345	330	140 135	2-3
Polysulfone (PSU)						3-4
Polyurethane (PU)	0.10	0.03	205	205	82	2-3
PU (elastomers)	0.07	0.03	200	205	100	2–3
<i>r</i> -PVC (polyvinyl chloride)	0.10	0.07	185	195	—	-
p-PVC (polyvinyl chloride)	0.02		175	150		
Styrene acrylonitrile (SAN)	0.03	0.02	215	245	82	3–4

While thermoplastic polymers soften at T_{g} , and if semicrystalline, melt at T_{m} cross-linked polymers do not melt and flow (Fig. 5.2 c^5). Lightly cross-linked polymers soften as the temperature exceeds T_{g} , but they remain rubbery solids until the polymer decomposes. Highly cross-linked polymers often do not even soften and retain a high modulus until reaching the decomposition temperature. Thermoset resins, like unsaturated polyester, epoxy, and polyurethanes, have varied levels of cross-linking. However, thermoplastic resins can be modified to contain few cross-links; lightly cross-linked polyethylene (XLPE) often improves the mechanical properties of rotomolded parts.

Some thermoplastics will decompose before they melt and flow. Extremely long polymer chains combined with intermolecular attractions prevent conventional melt processing of ultrahigh-molecular-

Robot Transfers Runner / Spru from Mold to Grinder

















